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TITLE: METHOD FOR COMPENSATION FOR A ZERO ERROR IN A
CORIOLIS GYRO

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BACKGROUND

5 Field of the Invention

The present invention relates to a Coriolis gyros. More particularly, this invention pertains to a method for compensation for a zero error in a Coriolis gyro.

10 Description of the Prior Art

Coriolis gyros (also referred to as "vibration gyros") are in increasing use for navigation. They possess a mass system that is caused to oscillate with the oscillation generally being the superposition of a large number of individual oscillations.

15 The individual oscillations of the mass system are initially independent of one another and can be referred to abstractly as "resonators". At least two resonators are required for operation of a vibration gyro:
20 one (the first resonator) is artificially stimulated to

oscillate, and this is referred to below as the
"stimulating oscillation". The other (the second
resonator) is stimulated to oscillate only when the
vibration gyro is moved/rotated. This is because Coriolis
5 forces occur in this case that couple the first resonator
to the second resonator, absorb energy from the
stimulating oscillation for the first resonator, and
transfer it to the read oscillation of the second
resonator. The oscillation of the second resonator is
10 referred to below as the "read oscillation".

In order to determine movements (in particular
rotations) of the Coriolis gyro, the read oscillation is
tapped off and a corresponding read signal (e.g. the read
oscillation tapped-off signal) is investigated to
15 determine whether any changes have occurred in the
amplitude of the read oscillation, as they represent a
measure of the rotation of the Coriolis gyro.

Coriolis gyros may be implemented as both open-
loop and closed-loop systems. In a closed-loop system,
20 the amplitude of the read oscillation is continuously
reset to a fixed value (preferably zero) by control

loops.

An example of a closed-loop version of a Coriolis gyro will be described below in conjunction Figure 2, a schematic diagram of a Coriolis gyro in accordance with the prior art. The gyro 1 includes a mass system 2 that can be caused to oscillate and is also referred to below as a "resonator". (A distinction exists between this expression and the abstract "resonators" term previously employed for individual oscillations of the "real" resonator. As mentioned, the resonator 2 may be considered as a system composed of two "resonators" (a first resonator 3 and a second resonator 4). Each of the first and the second resonators 3, 4 is coupled to a force sensor (not shown) and to a tapping system (not shown). The noise produced by the force sensor and the tapping systems is indicated schematically by Noise1 (reference symbol 5) and Noise2 (reference symbol 6).

The Coriolis gyro 1 includes four control loops. A first control loop controls the stimulating oscillation (that is to say the frequency of the first resonator 3) at a fixed frequency (resonant frequency). It comprises a

first demodulator 7, a first low-pass filter 8, a frequency regulator 9, a VCO (voltage controlled oscillator) 10 and a first modulator 11.

5 A second control loop controls the stimulating oscillation at constant amplitude. It comprises a second demodulator 12, a second low-pass filter 13 and an amplitude regulator 14.

10 Third and fourth control loops are employed to reset the forces that stimulate the read oscillation. The third control loop includes a third demodulator 15, a third low-pass filter 16, a quadrature regulator 17 and a third modulator 22 while the fourth control loop comprises a fourth demodulator 19, a fourth low-pass filter 20, a rotation rate regulator 21 and a second
15 modulator 18.

The first resonator 3 is stimulated at resonant frequency ω_1 . The resultant stimulating oscillation is tapped off, phase-demodulated by means of the first demodulator 7, and a demodulated signal component is
20 supplied to the first low-pass filter 8 that removes the

sum frequencies. (The tapped-off signal is also referred to below as the stimulating oscillation tapped-off signal.) An output signal from the first low-pass filter 8 is applied to a frequency regulator 9 which controls the VCO 10, as a function of the signal supplied to it, such that the in-phase component essentially tends to zero. The VCO 10 passes a signal to the first modulator 11, which controls a force sensor such that a stimulating force is applied to the first resonator 3. When the in-phase component is zero, the first resonator 3 oscillates at its resonant frequency ω_1 . (It should be noted that all of the modulators and demodulators are operated on the basis of resonant frequency ω_1 .)

The stimulating oscillation tapped-off signal is also applied to the second control loop and demodulated by the second demodulator 12. The output of the second demodulator 12 is passed through the second low-pass filter 13 whose output is, in turn, applied to the amplitude regulator 14. The amplitude regulator 14 controls the first modulator 11 in response to this signal and the output of a nominal amplitude sensor 23 to cause the first resonator 3 to oscillate at a constant amplitude

(i.e. the stimulating oscillation has constant amplitude).

As mentioned above, Coriolis forces (indicated by the term $FC \cos(\omega_1 \cdot t)$ in Figure 2) occur on movement/rotation of the Coriolis gyro 1. They couple the first resonator 3 to the second resonator 4, and thus cause the second resonator 4 to oscillate. A resultant read oscillation of frequency ω_2 is tapped off and a corresponding read oscillation tapped-off signal (read signal) is supplied to both the third and the fourth control loops. This signal is demodulated in the third control loop by the third demodulator 15, sum frequencies are removed by the third low-pass filter 16, and the low-pass-filtered signal is supplied to the quadrature regulator 17. The output of the quadrature regulator 17 is applied to the third modulator 22 to reset corresponding quadrature components of the read oscillation. Analogously, the read oscillation-tapped-off signal is demodulated in the fourth control loop by the fourth demodulator 19, passed through the fourth low-pass filter 20, and the low-pass-filtered signal then applied to the rotation rate regulator 21 (whose output is proportional to the instantaneous rotation rate, and

passed as a rotation rate measurement to a rotation rate output 24) and to the second modulator 18 that resets corresponding rotation rate components of the read oscillation.

5 A Coriolis gyro 1 as described above may be operated in both double-resonant and non-double-resonant forms. When operated in a double-resonant form, the frequency ω_2 of the read oscillation is approximately equal to that of the stimulating oscillation (ω_1). In
10 the non-double-resonant case, the frequency ω_2 of the read oscillation differs from ω_1 . In double resonance, the output signal from the fourth low-pass filter 20 contains corresponding information about the rotation rate. In contrast (non-double-resonant case), the output
15 signal from the third low-pass filter 16 contains the rotation rate information. In order to switch between the double-resonant and non-double-resonant operating modes, a doubling switch 25 selectively connects the outputs of the third and the fourth low-pass filter 16, 20 to the
20 rotation rate regulator 21 and the quadrature regulator 17.

As a result of unavoidable manufacturing tolerances, slight misalignments exist between the stimulating forces/resetting forces/force sensors/taps and the natural oscillations of the resonator 2 (i.e. the real stimulating and reading modes of the resonator 2). Such misalignments must be taken into account as the read oscillation tapped-off signal is otherwise subject to errors. In such a situation the read oscillation tapped-off signal thus includes a part that originates from the real read oscillation, and one that originates from the real stimulating oscillation. The undesired part causes a Coriolis gyro zero error of unknown magnitude as it is impossible to distinguish between these two parts when the read oscillation tapped-off signal is tapped off.

SUMMARY AND OBJECTS OF THE INVENTION

It is therefore an object of the invention to provide a method for compensating the above-described error.

The present invention provides, in a first aspect, a method for compensation for a zero error in a Coriolis gyro. In such method, the frequency of the read

oscillation is modulated. The output signal from a rotation rate control loop or quadrature control loop for the Coriolis gyro is demodulated in synchronism with the modulation of the frequency of the read oscillation to obtain an auxiliary signal which is a measure of the zero error. A compensation signal is then produced and passed to the input of the rotation rate control loop or quadrature control loop. The compensation signal is controlled so that the magnitude of the auxiliary signal is as small as possible.

In a second aspect, the invention provides a Coriolis gyro that includes a device for determination of zero error. Such device includes a modulation unit that modulates the frequency of the read oscillation of the Coriolis gyro. A demodulation unit demodulates the output signal from a rotation rate control loop or quadrature control loop in synchronism with modulation of the frequency of the read oscillation to obtain an auxiliary signal that is a measure of the zero error. A control unit produces a compensation signal and passes it to the input of the rotation rate control loop or quadrature control loop. The control unit controls the compensation

signal so that the auxiliary signal is as small as possible.

The foregoing and other features of the invention will become further apparent from the detailed description that follows. Such description is accompanied
5 by a set of drawing figures. Numerals of the drawing figures, corresponding to those of the written description, point to the features of the invention with like numerals referring to like features throughout both
10 the drawing figures and the written description.

BRIEF DESCRIPTION OF THE DRAWINGS

Figure 1 is a schematic diagram of a Coriolis gyro in accordance with the invention;

Figure 2 is a schematic diagram of a Coriolis gyro in accordance with the prior art;
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Figure 3 is a vector diagram for illustrating the interaction of the resonator, force sensor system and tapping system in a Coriolis gyro;

Figures 4a through 4d are a set of vector diagrams for illustrating forces and oscillation
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amplitudes for a Coriolis gyro at double resonance;

Figures 5a through 5d are a set of vector diagrams for illustrating forces and oscillation amplitudes for a Coriolis gyro close to double resonance;

5 Figures 6a through 6d are a series of vector diagrams for illustrating the method according to the invention at double resonance; and

Figures 7a through 7d are a series of vector diagrams for illustrating the method according to the invention close to double resonance.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENT

The general method of operation of a Coriolis gyro is explained again with reference to the vector diagrams of Figures 3 to 5 (Gaussian number plane). The method of the invention functions only at essentially double resonance (on average). Drawings labeled "close to double resonance" illustrate the changed conditions when the situation of "close to double resonance" occurs as a result of modulation of the resonant frequency of the read oscillation.

The vector diagram of Figure 3 illustrates a Coriolis gyro (system 40) comprising a resonator (not shown), a force sensor system 41 and a tapping system 42. Possible oscillations x (stimulation) and y (read) are also indicated. Such oscillations are coupled to one another by Coriolis forces in the event of rotation at right angle to the plane of the drawing. The x oscillation (complex; purely imaginary at resonance) is stimulated by an alternating force with the complex amplitude F_x (in this case only the real part of F_{xr}). The y oscillation (complex) is reset by an alternating force of complex amplitude F_y with the real part F_{yr} and the imaginary part F_{yi} . (The rotation vectors $\exp(i\omega t)$ are omitted in each case).

Figures 4a to 4d illustrate the forces and oscillation amplitude for a Coriolis gyro at double resonance. That is they show the complex forces and complex oscillation amplitudes for an ideal Coriolis gyro with the same resonant frequency for the x and y oscillations. The force F_{xr} is controlled to produce a purely imaginary, constant x oscillation. This is achieved by the amplitude regulator 14 (which controls the

magnitude of the x oscillation) and the phase regulator
10/frequency regulator 9 (which controls the phase of the
x oscillation). The operating frequency ω_1 is controlled
so that the x oscillation is purely imaginary (i.e. the
5 real part of the x oscillation is controlled to be zero).

The Coriolis force during rotation, FC , is now
purely real, since it is proportional to the speed of the
x oscillation. If both oscillation have the same resonant
frequency, then the y oscillation, caused by the force FC ,
10 has the form illustrated in Figure 4d. If the resonant
frequencies of the x and y oscillations differ slightly,
then complex forces and oscillation amplitudes occur as
illustrated in Figures 5a to 5d. In particular, this
results in a y oscillation, stimulated by FC , as shown in
15 Figure 5d.

When double resonance is present, the real part
of the y tapped-off signal is zero. It is not zero in the
absence of double resonance. In both cases, with reset
gyros, the Coriolis force FC is zeroed by a regulator F_{yr}
20 which comprises FC . In the case of Coriolis gyros

operated with double resonance, the imaginary part of y is zeroed by F_{yr} , and the real part of y is zeroed by F_{yi} . The bandwidths of the two control processes are approximately 100 Hz.

5 Figure 1 is a schematic diagram of a Coriolis gyro in accordance with the invention. Parts corresponding to those of the prior art gyro of Figure 2 are annotated with the same reference symbols and not again explained. The resetting Coriolis gyro 1' of Figure 10 includes a demodulation unit 26, a fifth low-pass filter 27, a control unit 28, a modulation unit 29 and a first multiplier 30 or, alternatively, a second multiplier 31. The modulation unit 29 modulates the frequency of the read oscillation of the resonator 2 at ω_{mod} . An output signal 15 from the quadrature control loop is supplied to the demodulation unit 26. It demodulates this signal in synchronism with the frequency ω_{mod} to obtain an auxiliary signal. Should there be any zero error (i.e. due, for example, to misalignments between the stimulating 20 forces/resetting forces/force sensors/taps and the natural oscillations of the resonator 2) the strength of the auxiliary signal will then vary as a function of the

frequency of the read oscillation.

The auxiliary signal is supplied to the fifth low-pass filter 27, which produces a low-pass-filtered signal and supplies it to the control unit 28. The control unit 28 employs the low-pass-filtered auxiliary signal to produce a signal which is applied to the first multiplier 30. This multiplies the signal emitted from the control unit 28 by a signal that originates from the amplitude regulator 14 to control the amplitude of the stimulating oscillation.

A compensation signal, obtained from the multiplication process, is added to the input to the rotation rate control loop. The control unit 28 controls the signal supplied to the first multiplier 30 so that the magnitude of the auxiliary signal is as small as possible. This corrects the zero error. The magnitude of the zero error can be determined by the compensation signal, which represents a measure of the zero error. Alternatively, the output signal from the control unit 28 can be supplied to the second multiplier 31, which multiplies this signal

by the stimulating oscillation tapped-off signal and adds a compensation signal, produced in this way, to the read oscillation tapped-off signal. (The expression "control unit" is not restricted to the control unit 28 but may also mean the combination of the control unit 28 and the first or second multiplier 30,31). The signal supplied to the demodulation unit 26 may alternatively be tapped-off at a different point within the control loops.

The method of the invention can also be illustrated with reference to Figures 6a to 6d and 7a to 7d. The tap for the y oscillation (second resonator x2, 4) in general also "sees" a part of the x oscillation (first resonator x1, 3): $a_{21} \cdot x$. This produces a Coriolis gyro zero error (to be determined). Figures 6a through 6d illustrate the situation at double resonance, while Figures 7a through 7d illustrate the situation at close to double resonance. In both cases, the sum signal of the actual y movement and $a_{21} \cdot x$ is "zeroed" by means of F_{yi} and F_{yr} . If a_{21} is not equal to zero, F_{xr} is not equal to zero when the rotation rate is zero (zero error). F_{yi} becomes zero only when double resonance is present. A quadrature bias results when there are discrepancies in

the resonant frequencies.

Compensation for a_{21} is accomplished, according to the invention, as follows. The gyro is assumed to be at double resonance. The resonant frequency of the read oscillation (which can be electronically detuned) is modulated by the modulation unit 29 with a zero mean value (e.g. 55 Hz). The signal F_{yi} is demodulated by the demodulation unit 26 in synchronism when the resetting control loops are closed. If a_{21} were zero, then F_{yi} would not vary with frequency. That is, it changes only where a_{21} is not equal to zero. In the latter case, the low-pass-filtered, synchronously demodulated F_{yi} signal is not zero. The demodulated signal is supplied to the control unit 28 (preferably in the form of software), which controls a factor a_{21comp} (auxiliary variable). A controlled component of the x movement, $a_{21comp} \cdot x$, is tapped off from the signal at the y tap (preferably in software). The magnitude of the component a_{21comp} is controlled so that the demodulated F_{yi} signal becomes zero. There is, therefore, no longer any x signal component in the signal from the y tap that has been cleaned in this way and the bias due to read cross-

coupling disappears. At double resonance and with the same Q factors, a cross-coupling regulator would zero the bias caused by the read cross-coupling on its own. This is due to the fact that the modulation of F_{xr} also
5 slightly modulates the amplitude of x . The sum of the force component of x in F_{yr} and the read component of x at the y tap is thus zeroed via the force cross-coupling regulator. The bias therefore disappears if the Q factor is the same.

10 It is also possible to use noise to modulate the read oscillation. Appropriate synchronous demodulation of the noise component in the read signal is then employed.

One major discovery on which the invention is based is that the output signal from the rotation rate
15 control loop/quadrature control loop changes as a result of a change in the frequency of the read oscillation only when there is a corresponding zero error (i.e. when misalignments exist between the stimulating
forces/resetting forces/force sensors/taps and the natural
20 oscillations of the resonator). Thus, if a compensation signal that compensates for the zero error in the read

oscillation tapped-off signal caused by misalignments is
passed to the input of the rotation rate control
loop/quadrature control loop, or directly to the read
oscillation tapped-off signal, the output signal from the
rotation rate control loop/quadrature control loop does
not change further in the event of a change in the
frequency (in particular, a change in the resonant
frequency) of the read oscillation. Since the change in
the output signal from the rotation rate control
loop/quadrature control loop is recorded by the auxiliary
signal, the zero error can be determined and compensated
for by controlling the compensation signal so that the
auxiliary signal (and, thus, the change in the output
signal from the control loop) is as small as possible.
The frequency (resonant frequency) of the read oscillation
is preferably modulated with zero mean value (e.g. at 55
Hz).

While this invention has been illustrated with
reference to its presently-preferred embodiment, it is not
limited thereto. Rather, the invention is limited only
insofar as it is defined by the following set of patent
claims and includes within its scope all equivalents

thereof.